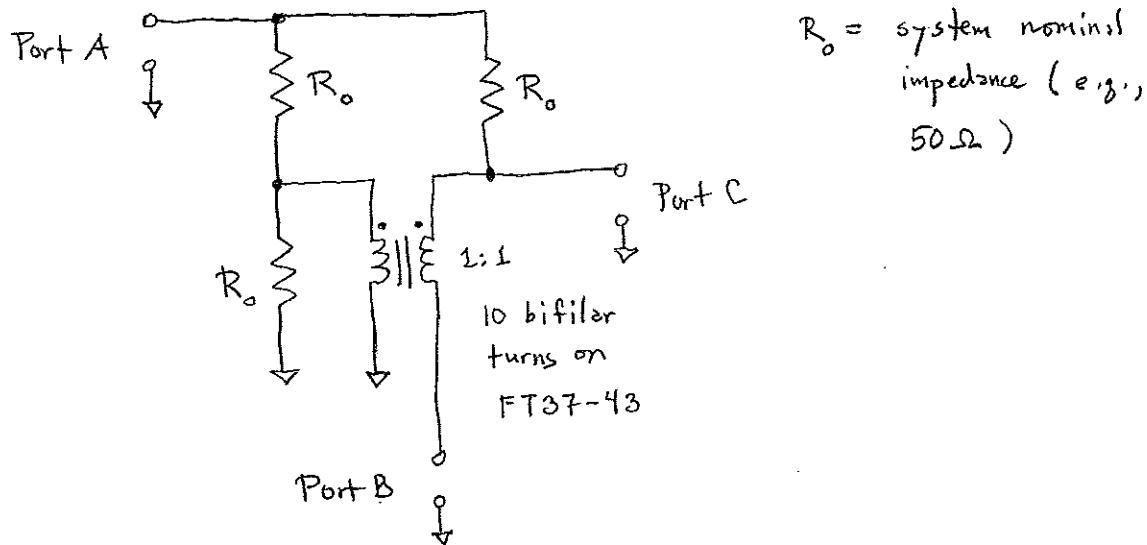


# One Circuit, Three Uses - The RLB (Return Loss Bridge)

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I ran across this circuit in a college textbook on analog radio circuits, then found it in Experimental Methods in RF Design (EMRFD), Ch. 7. (The two circuits differ slightly but perform identically except as a splitter.)



Here are the three uses. (We only use signal sources and terminations with impedance  $R_o$ .)

## Combiner (Linear mixer)

Port A : Signal source 1 , power  $P_1$  input

Port B : Signal source 2 , power  $P_2$  input

Port C : Sum of input signals with power  $\frac{P_1 + P_2}{4}$  output  
(6 dB attenuation)

Theoretically, no power from Port A will enter Port B and vice versa, so they have perfect isolation from each other.

## Splitter

Port C: Signal source, power  $P$  input

Port A: Same as source, power  $P/4$  ( $6 \text{ dB}$  attenuation) output

Port B: Same as Port A

With the circuit shown (EMRFD version) the two outputs are in phase. If the lower connections on the transformer are switched (textbook version), the two outputs are  $180^\circ$  out of phase.

## Return Loss Bridge

Port A: Signal source

Port B: Detector (voltmeter, power meter, or oscilloscope)

Port C: Device under test (DUT) with unknown impedance  $Z$

The detector measures the power (or voltage) reflected by the impedance. The basic procedure is as follows:

1. Leave Port C open (disconnected) and measure the power  $P_{oc}$  or voltage  $V_{oc}$  at Port B.

2. Connect the DUT to Port C and measure the power  $P_{DUT}$  or voltage  $V_{DUT}$  at Port B.

3. Calculate

$$\rho = |\text{reflection coefficient } \Gamma| = \left| \frac{Z - R_0}{Z + R_0} \right|$$

$$= \frac{V_{DUT}}{V_{oc}} = \sqrt{\frac{P_{DUT}}{P_{oc}}}$$

$$\text{Return loss } RL = -20 \log_{10} \rho$$

~~Because an open (or short) reflects all power,  $V_{oc}$  is the (forward) power going to the DUT when it is connected to Port C. Thus.~~

$\rho = \frac{V_{DUT}}{V_{oc}}$  is the ratio (of the magnitudes) of the reflected to forward voltages.

The VSWR can be easily calculated from  $\rho$  by the equation

$$VSWR = \frac{1 + \rho}{1 - \rho}$$

$\rho$	0	0.0100	0.1000	0.3311	0.5623	0.7943	0.8913	1
$R_L$	$+\infty$	40	.20	9.6	5	2	1	0
VSWR	1	1.02	1.22	1.99	3.57	8.72	17.39	$+\infty$

This table gives an idea of the relationships among these three ways of quantifying impedance mismatches between  $Z$  and  $R_o$ .

### Quality of a RLB

How well an RLB measures reflected power is expressed by two quantities:

Directivity =  $R_L$  measured when a precision matched termination  $R_o$  is put at Port C as the DUT.

The higher the better for directivity. Bridges with at least 40 dB are considered acceptable.

O/S Ratio =  $20 \log \frac{V_{oc}}{V_{sc}}$  where  $V_{oc}$  = voltage at Port B

for an open circuit DUT,  $V_{sc}$  = same for short circuit

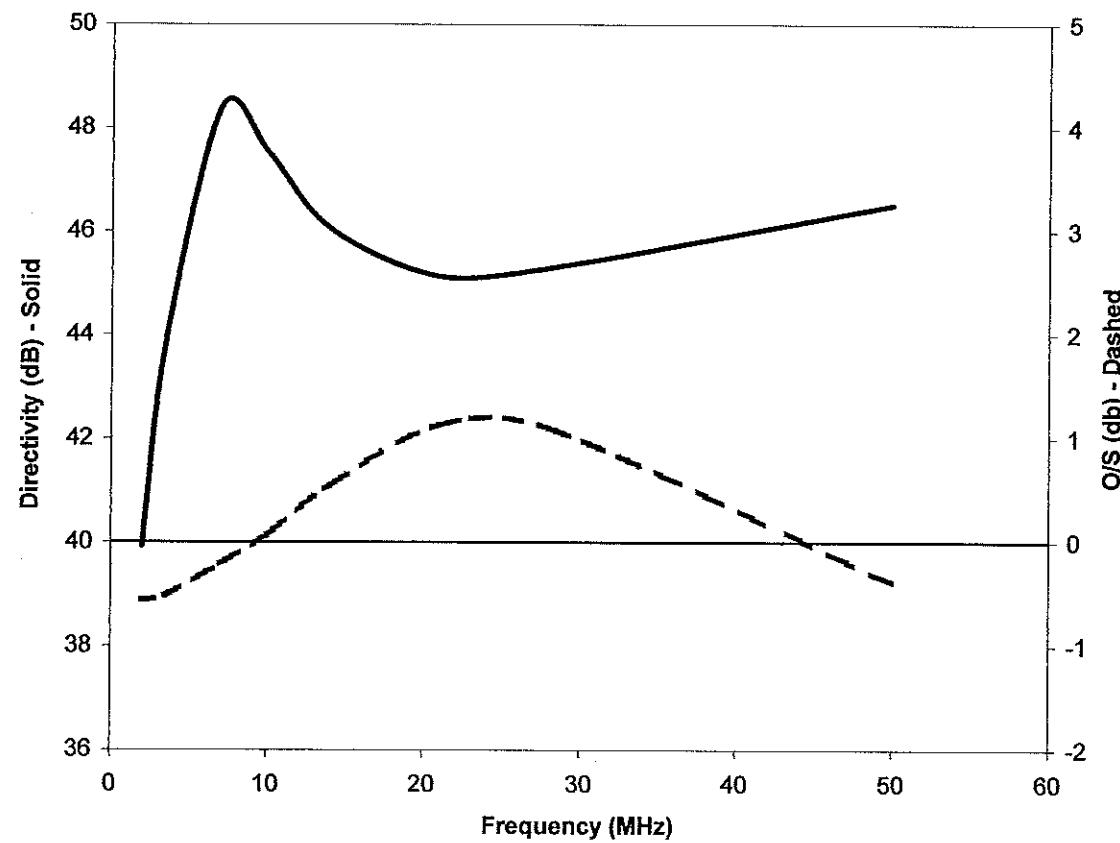
Ideally this value is zero, since a short and open should reflect all power.

Nominal voltage values

Gen V            6 V  
 V in            3 V  
 $V_{OPEN}$         750 mV

Freq f MHz	$V_{OPEN}$ mV <sub>pp</sub>	$V_{SHORT}$ mV <sub>pp</sub>	O/S dB	Har Avg mV <sub>pp</sub>	$V_{Matched}$ mV <sub>pp</sub>	$\rho$	Dir dB	VSWR
2	720	768	-0.56	743.6	7.5	0.010086	39.9	1.020
3.5	718	762	-0.52	739.7	4.75	0.006422	43.8	1.013
7	728	746	-0.21	736.9	2.8	0.003799	48.4	1.008
10	740	734	0.07	737.0	3.1	0.004206	47.5	1.008
14	756	710	0.55	732.6	3.65	0.004982	46.1	1.010
21	780	685	1.13	731.0	4.05	0.005541	45.1	1.011
28	774	682	1.10	726.5	3.95	0.005437	45.3	1.011
50	704	736	-0.39	719.8	3.4	0.004723	46.5	1.009

### Directivity and O/S of Homebrew RLB



The previous page shows the directivity and O/S ratio for the bridge I made. Its values are reasonable over HF to 6m frequencies.

The directivity values come from some signal forward power sneaking into the detector port. Some tedious math gives us limits on the measurement error due to finite directivity. They are shown on the next page for an RL<sub>B</sub> with 40 dB directivity.

The plot shows that measurements are practical for return losses of 35 dB and lower (greater mismatch). This is plenty for  $\approx$  perfect match (VSWR 1.04 : 1)!

### Messuring Impedance $Z$ with $\approx$ RL<sub>B</sub>

This can be done using two known impedances (e.g.  $\approx$  resistor and  $\approx$  capacitor). Measure  $P$  or RL for:

1. The DUT alone
2. The DUT in series with Known 1
3. The DUT in series with Known 2

For each of these we get a circle in the impedance plane. Where the three circles intersect each other gives the unknown impedance  $Z$ . The math details are  $\approx$  bit messy.

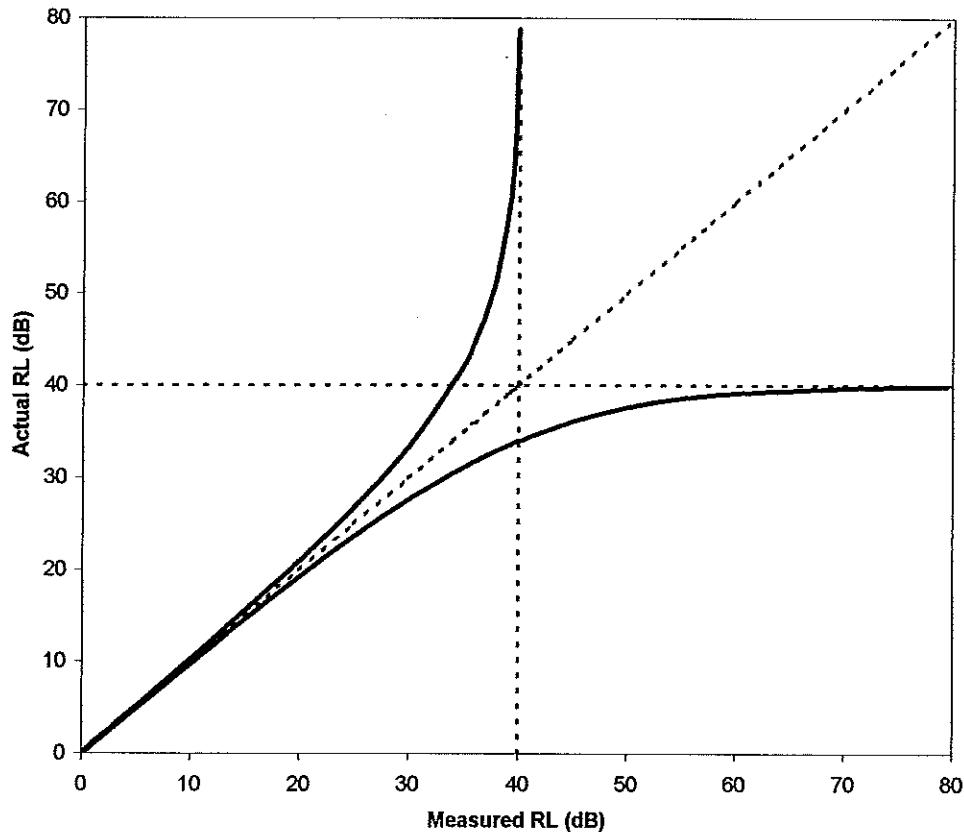
The last two pages show how well this worked using my RL<sub>B</sub> and two unknowns,  $\approx$  98.4 Ω resistor (100 Ω nominal) and that same resistor in series with  $\approx$  100 pF capacitor.

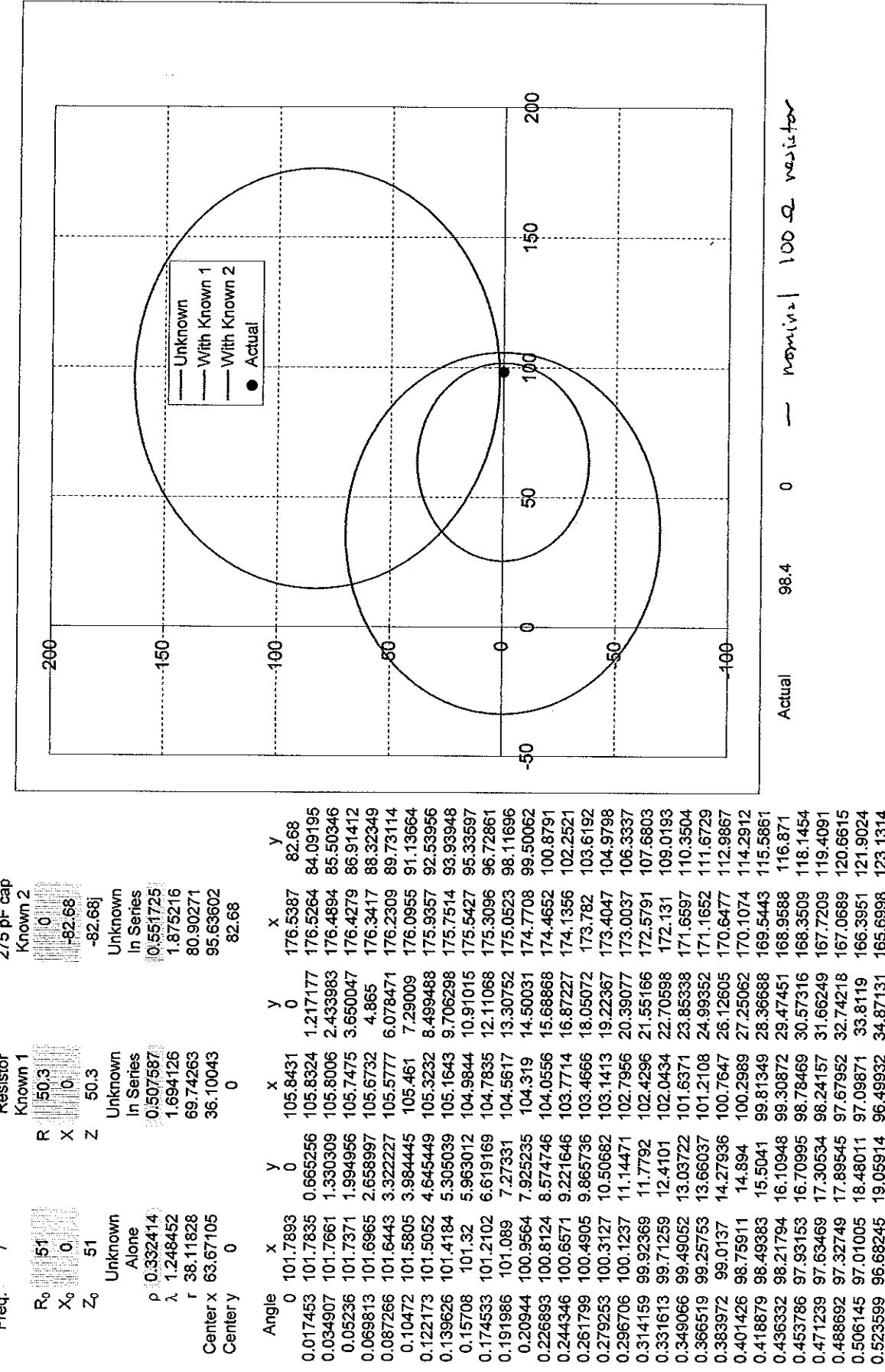
The measurements were done at 7 MHz where my bridge had the best directivity and O/S ratio.

## Directivity 40

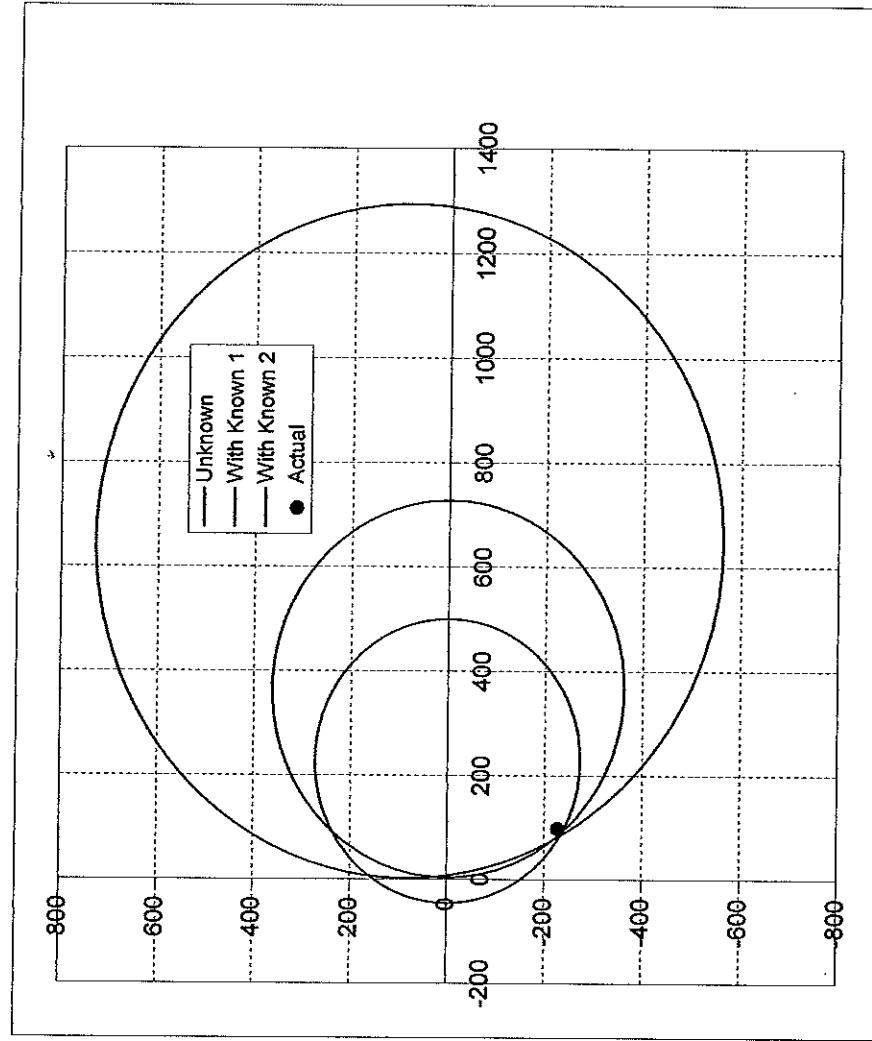
RL Measured	p	VSWR	RL Lower Bound	RL Upper Bound
0.1	0.9886	173.72	0.0	0.2
1	0.8913	17.39	0.9	1.1
2	0.7943	8.72	1.9	2.1
5	0.5623	3.57	4.8	5.2
9.6	0.3311	1.99	9.3	9.9
15	0.1778	1.43	14.5	15.5
20	0.1000	1.22	19.2	20.9
25	0.0562	1.12	23.6	26.7
30	0.0316	1.07	27.6	33.3
35	0.0178	1.04	31.1	42.2
				Practical range limit
36	0.0158	1.03	31.8	44.7
37	0.0141	1.03	32.4	47.7
38	0.0126	1.03	32.9	51.7
39	0.0112	1.02	33.5	58.3
39.3	0.0108	1.02	33.6	61.5
39.6	0.0105	1.02	33.8	66.5
39.9	0.0101	1.02	33.9	78.7
40	0.0100	1.02	34.0	
45	0.0056	1.01	36.1	
50	0.0032	1.01	37.6	
55	0.0018	1.00	38.6	
60	0.0010	1.00	39.2	
70	0.0003	1.00	39.7	
79.5	0.0001	1.00	39.9	

Directivity Error for RL Measurement, Directivity = 40 dB





Freq.	7	Resistor Known 1	275 pF cap Known 2
$R_0$	5	R 50.3	0
$X_0$	0	X 0	-82.68
$Z_0$	51	Z 50.3	-82.68
Unknown Alone		Unknown In Series	Unknown In Parallel
P 0.869966		0.830346	0.924139
$\lambda$ 7.166682		5.440681	12.70168
r 361.9252		272.7776	645.7752
Center x 365.5008		227.1747	647.7859
Center y 0		0	82.68
Angle x	x	y	x
0	727.426	0	499.9223
0.017453	727.3708	6.316465	499.8808
0.034907	727.2055	12.63101	499.7562
0.05236	726.93	18.9417	499.5485
0.069813	726.5443	25.24662	499.2979
0.087266	726.0487	31.54386	498.8844
0.10472	725.4433	37.83148	498.4282
0.122173	724.7282	44.10758	497.8893
0.139626	723.9037	50.37025	497.2668
0.15708	722.9701	56.61757	496.5643
0.174533	721.9275	62.84765	495.7787
0.191986	720.7764	69.05858	494.9112
0.20944	719.517	75.24847	493.9621
0.226893	718.1498	81.41545	492.9318
0.244346	716.6752	87.55762	491.8205
0.261799	715.0937	93.67313	490.6287
0.279253	713.4056	99.7601	489.3565
0.296706	711.6116	105.8167	488.09345
0.314159	709.7121	111.841	486.5731
0.331613	707.7078	117.8313	485.0626
0.349066	705.5992	123.7857	483.4736
0.366519	703.387	129.7024	481.8065
0.383972	701.072	135.5796	480.0619
0.401426	698.6547	141.4154	478.2402
0.418879	696.1359	147.2082	476.342
0.436332	693.5164	152.9562	474.368
0.453786	690.797	158.6576	472.3186
0.471239	687.9785	164.3106	470.1946
0.488692	685.0618	169.9336	467.9966
0.506145	682.0477	175.4648	465.7251
0.523559	678.9372	180.9626	463.3811



Actual 98.4 -227.4 — nominal 100  $\Omega$  resistor in series with 100  $\Omega$  capacitor

at 7 MHz